Proceedings of the XXIII Conference on Applied Crystallography, Krynica Zdrój, Poland, September 20–24, 2015

Semi-Conducting Properties of Titanium Dioxide Layer on Surface of Ti–15Mo Implant Alloy in Biological Milieu

M. SZKLARSKA^{*a*}, G. DERCZ^{*a*}, J. KUBISZTAL^{*a*}, K. BALIN^{*b*} AND B. ŁOSIEWICZ^{*a*,*} ^{*a*}Institute of Materials Science, University of Silesia, 75 Pułku Piechoty 1A, 41-500 Chorzów, Poland ^{*b*}A. Chełkowski Institute of Physics, University of Silesia, Uniwersytecka 4, 40-007 Katowice, Poland

The object of this work was to investigate structure, electrochemical behavior and semiconducting properties of the TiO_2 oxide layer on the Ti-15M implant alloy surface in normal and inflammatory conditions of physiological saline solution. X-ray photoelectron spectroscopy measurements confirm the presence of the oxide layer on the Ti-15M alloy surface. Electrochemical studies indicate excellent corrosion resistance of Ti-15M alloy in physiological saline solution. It was found that the investigated material under normal and inflammatory conditions behave like an insulator and *n*-type semiconductor, respectively.

DOI: 10.12693/APhysPolA.130.1085

PACS/topics: 87.85.jj, 82.45.Bb, 72.20.-i

1. Introduction

Titanium and its alloys with mechanical properties similar to the human bones, low weight and Young modules, high biocompatibility, biological inertness, and good corrosion resistance are excellent materials for biomedical applications [1–4]. Among these materials, a Ti-15Mo alloy can be distinguished. Addition of Mo increases the corrosion resistance simultaneously reducing the elastic modulus [4]. Moreover, because of the high oxygen affinity of Ti and its alloys, the Ti-15Mo alloy is self-passivated material and is covered with a stable oxide layer which is strongly adherent to the surface and protects it against harmful environmental factors, e.g. human body [3, 5]. In many cases the implementation of dental or orthopaedic device provokes an inflammatory response of human body. During the inflammation the amount of hydrogen peroxide is growing, pH level is decreasing, and these changes can strongly affect corrosion behavior of the implants [6–8]. Therefore, the aim of this study is to examine structure, electrochemical behavior, and semiconducting properties of the oxide layer on the Ti-15Mo implant alloy in physiological saline solution (PSS) under normal and inflammatory conditions.

2. Experimental

Phase composition of the Ti–15Mo implant was tested by X-ray diffraction with the use of an X-ray X'Pert diffractometer manufactured by Phillips, with copper target X-ray tube ($\lambda = 1.54$ Å) operated at 40 kV and 30 mA. Cu K_{α} radiation was monochromatized with a graphite monochromizer. Wide angle X-ray scattering (WAXS) curves were recorded in a step scanning mode, over a diffraction angle (2θ) range: $20^{\circ}-140^{\circ}$, with the step of 0.05° .

Chemical composition of thin oxide layer spontaneously formed on the Ti-15Mo surface has been studied towards X-ray photoelectron spectroscopy (XPS). The XPS measurements were realized with the use of VG-Scienta & Prevac spectrometer. Monochromatized Al K_{α} radiation was used to obtain the photoelectron spectra of Mo 3d, Ti 2p, O 1s and C 1s before and after the sputtering process (Ar⁺ ions, 9 mA, 4 kV, 20 min). The electrochemical measurements were carried out in electrochemical cell described previously [3] in a PSS of 0.9% NaCl solution of $pH = 7.4 \pm 0.1$ at 37 ± 1 °C and in PSS with 15 mM H_2O_2 solution of pH = 4.5 ± 0.1 (titrated HCl) at 40 ± 1 °C to simulate normal and inflammatory physiological conditions in human body, respectively. Electrical properties of the oxide layer were analysed by anodic polarization and electrochemical impedance spectroscopy (EIS) methods using the Metrohm/Eco Chemie Autloab PGSTAT30 potentiostat/galvanostat electrochemical system. The E_{OC} was stabilized for 2 h. Based on the anodic polarization curves, the potential range from +5 V to -0.3 V vs. saturated calomel electrode (SCE) for EIS measurements was selected. Impedance spectra registered potentiostatically at frequencies of 50 kHz-0.1 Hz were approximated using the EQUIVCRT program. Scanning Kelvin probe (SKP) measurements were used to obtain the topography map of the sample and to determine the changes in the distribution of contact potential difference on the bottom of corrosion pit and surface of Ti-15Mo sample. The SKP tests were conducted using scanning electrochemical workstation M370.

3. Results and discussion

The X-ray analysis confirmed that the Ti15Mo implant alloy contained only β -Ti phase (ICDD PDF 01-089-4913) which improves corrosion resistance and mechanical properties. Moreover, excellent corrosion resistance of the Ti-15Mo alloy is also provided by presence of stable, spontaneously formed on air, oxide layer on its

^{*}corresponding author; e-mail: bozena.Łosiewicz@us.edu.pl

surface. The XPS was used to determine the oxidation states of Ti and Mo on the surface of the Ti-15Mo alloy. The survey spectra obtained before and after the sputtering process showed principal core levels of Ti, Mo, O and C (the last one significantly removed during the sputtering process). The atomic concentration calculations before and after sputtering process indicate uniform ratio of Ti/Mo, which confirms homogenous distribution of Ti and Mo on subsurface layers of the alloy. The analysis of chemical states of Ti and Mo, obtained from detailed analysis of the Ti 2p and Mo 3d multiplets (Fig. 1), indicated that both elements, before and after sputtering process, exhibit metallic as well as oxide nature. The low binding energy states of Ti determined for Ti $2p_{2/3}$ were at 454.58 eV before the sputtering process and at 454.7 eV after sputtering process. In case of low binding energy states of Mo, here given for Mo $3d_{5/2}$ were obtained at 227.75 eV before sputtering process and at $227.9~\mathrm{eV}$ after the sputtering process. Both results indicate presence of Ti and Mo in metallic state. Presence of metallic states of Ti and Mo before sputtering process indicates that the oxide layer formed on the surface is not continuous (incomplete coverage or mixture of oxide and metallic states). The peaks of higher binding energies are assigned to various forms of oxides. Before the sputtering process the Ti $2p_{3/2}$ peak at 460 eV, and Mo $3d_{5/2}$ at 230.42 eV indicate presence of nonstoichiometric TiO₂ and MoO₂ oxides. Other forms of oxides such as stoichiometric TiO₂ and MoO₂ (Ti $2p_{3/2}$ at 458.24 eV, and Mo $3d_{5/2}$ at 229.76 eV) or assigned to MoO₃ peak at 232.73 eV are also present. After the sputtering process the tendency for both elements is similar — the amount of nonstoichiometric TiO₂ and MoO₂ have been reduced, and some new intermediate oxides appeared (Fig. 1). This indicates that the oxidation process was in some way gradual.



Fig. 1. High-resolution XPS spectra of the Ti2p and Mo3d levels obtained before and after the sputtering process. The raw data spectra (black) are fitted with several components assigned to particular chemical states as marked in the legend.



Fig. 2. Bode plots for Ti–15Mo implant alloy at E_{OC} for normal and inflammatory conditions.

All impedance spectra registered towards corrosion behavior and semi-conducting properties of the Ti-15Mo alloy were approximated using the modified Randle's cell [9] which represents the physical model of the Ti-15Mo|TiO₂ film|PSS system. The constant phase element (CPE) was used instead of a capacitor. The results of EIS measurements conducted at E_{OC} for the neutral and inflammatory state, were presented in Bode diagrams (Fig. 2). Bode-phase plots show one time constant characteristic for the oxide layer presence on the metallic substrate. The value of $\log |Z|_{f=0.1\text{Hz}}$ for the neutral and inflammatory state is 5.51 ± 0.49 and $4.84 \pm 0.49 \ \Omega \text{cm}^2$, respectively. It suggests that presence of additional chloride ions and increasing temperature of the solution increase the probability of occurrence the pitting corrosion at inflammatory state. Mott-Schottky (M-S) analysis of capacitance parameter determined in EIS tests allowed to determine the type of semi-conductivity and carrier concentration in the oxide layer. The donor density, N_D , and flat band potential, V_{fb} , were calculated from the Eq. (1) [10]:

$$\frac{1}{C^2} = \frac{2}{\varepsilon_{\text{TiO}_2}\varepsilon_0 A^2 e N_D} \left(V - V_{fb} - \frac{k_{\text{B}}T}{e} \right), \tag{1}$$

where: C is the capacitance, $\varepsilon_{\text{TiO}_2}$ is the dielectric constant of TiO₂, $\varepsilon_0 = 8.85 \times 10^{-14}$ F/cm is permittivity of free space, e is the elementary charge $(1.6 \times 10^{-19} \text{ C})$, A is the tested surface area, V is the voltage of the interface, k_{B} is the Boltzmann constant, and T is a temperature. The M-S plot for neutral conditions shows a flat area at potential of 0.3–4.5 V indicating that investigated material behaves like insulator (Fig. 3). Whereas the positive slope of the curve $1/C^2 = f(E)$ in Fig. 3 points the n-type semi-conductivity with carrier concentration of $N_D = 5.84 \times 10^{18} \text{ cm}^{-3}$ and $V_{fb} = -4.97$ for the Ti–15Mo alloy exposed to inflammatory conditions.

Anodic polarization measurements indicate slightly better corrosion resistance of the Ti–15Mo alloy at in-



Fig. 3. Mott–Schottky plots for Ti–15Mo at normal and inflammatory conditions.



Fig. 4. Anodic potentiodynamic curve for Ti–15Mo alloy in PSS.



Fig. 5. Topography of corrosion pit on Ti–15Mo surface obtained by the SKP method.

flammatory conditions (Fig. 4). It is evidenced by the lower current density for inflammation state. However significant increase in current density at potential of 8 V indicates that brake-down of protection oxide layer has occurred and pitting corrosion had started. SKP measurements allowed to determine the corrosion pit depth of 87 μ m. This method also revealed that the corrosion pit has a shape of hopper with the diameter of 2000 μ m and 500 μ m at the hopper top and bottom, respectively (Fig. 5). Measurements of contact potential difference indicate that the bottom of corrosion pit has lower corrosion resistance than the surrounding surface.

4. Conclusions

Electrochemical behavior of oxide layer present on the Ti–15Mo implant alloy is strongly dependent on the occurrence of inflammation in human body. At normal conditions oxide layer behaves as an insulator whereas at inflammatory conditions it shows n-type semi-conductivity with carrier concentration $N_D = 5.84 \times 10^{18}$ cm⁻³. This behavior is caused by addition of H₂O₂ into solution and increase in temperature and number of chloride ions. It could be the reason that more defected oxides are formed on the examined alloy surface which affect the semiconducting properties and also influence decreasing of corrosion resistance of Ti–15Mo in biological milieu at inflammatory state.

References

- J. Lelątko, T. Goryczka, T. Wierzchoń, M. Ossowski, B. Łosiewicz, E. Rówinski, H. Morawiec, *Solid State Phenom.* 163, 127 (2010).
- [2] A. Smołka, K. Rodak, G. Dercz, K. Dudek, B. Łosiewicz, *Acta Phys. Pol. A* **125**, 932 (2014).
- [3] M. Szklarska, G. Dercz, W. Simka, B. Łosiewicz, Surf. Interface Anal. 46, 698 (2014).
- [4] W. Simka, A. Krząkała, D.M. Korotin, I.S. Zhidkov, E.Z. Kurmaev, S.O. Cholakh, K. Kuna, G. Dercz, J. Michalska, K. Suchanek, T. Gorewoda, *Electrochim. Acta* 96, 180 (2013).
- [5] M. Freitag, B. Łosiewicz, T. Goryczka, J. Lelątko, Solid State Phenom. 183, 57 (2012).
- [6] P. Handzlik, K. Fitzner, Trans. Nonferrous Met. Soc. China 23, 866 (2013).
- [7] E. Brooks, M. Tobias, K. Krautsak, M. Ehrensberg, J. Biomed. Mater. Res. B 102, 1445 (2014).
- [8] I.M. Pohrelyuk, V.M. Fedirko, O.V. Tkachuk, R.V. Proskurnyak, *Corros. Sci.* 66, 392 (2013).
- [9] A.S. Bondarenko, G.A. Ragoisha, J. Solid State Electrochem. 9, 845 (2005).
- [10] M. Szklarska, G. Dercz, J. Rak, W. Simka, B. Łosiewicz, Archiv. Metall. Mater. 4, 2687 (2015).