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Effect of Filler Mixture Ratio on Permeability of Multicomponent Soft Magnetic Composites

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Composites with hybrid LiZnTi ferrite/FeSiAl alloy filler and PVC polymer matrix were synthesized by thermal pressing process. The influence of the mixture ratio of hybrid filler on the frequency dispersion of complex permeability of the composites has been studied. The dispersion of permeability varied from resonance type to relaxation one with the configuration change from LiZnTi/PVC composite to FeSiAl/PVC one and was mainly due to the magnetic resonance phenomena such as domain wall and spin precession resonance and due to the eddy current effect.

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1. Introduction

Recently, composite materials consisting of magnetic fillers in a host polymer matrix have attracted much attention due to their value for extensive applications at high frequency in industry, commerce and defense. Compared with ferrite fillers, metallic magnetic fillers have higher saturation magnetization and the Snoek's limit exists at a high frequency side [1, 2]. However, their permeability decreases dramatically in GHz range since eddy currents induced by high frequency irradiation increase rapidly due to high electrical conductivity. Soft ferrite fillers are insulating materials, so the composites of soft ferrites and metallic magnetic materials can be better alternatives. The aim of this report is to synthesize LiZnTi/FeSiAl/PVC composites and analyze their frequency variation of complex permeability in the broad frequency range (1 MHz-6.5 GHz).

2. Experimental

LiZnTi ferrite of composition $Li_{0.525}Zn_{0.30}Ti_{0.35}$ $Fe_{1.825}O_4$ (synthesized by a ceramic route at $1050~^\circ\mathrm{C}/3.5$ h in air) and a commercially available FeSiAl alloy (Kovohuty Co., Dolný Kubín, Slovakia) of composition $Fe_{82.5}Si_{15.0}Al_{0.3}$ (the rest to balance present Mn, Cr and C with amount less than 1%) in bulk and also powder form were used as magnetic fillers. The particle size of fillers was controlled under 250 μ m for LiZnTi ferrite and under 160 μ m for FeSiAl alloy, respectively. The powder fillers were uniformly mixed with polyvinylchloride (PVC) at a constant total filler volume content of 60 vol%. The mixture ratio of hybrid LiZnTi:FeSiAl filler was set to 1:0, 0.75:0.25, 0.50:0.50, 0.25:0.75, and 0:1. Ring shaped composite samples (outer diameter 7.9 mm, inner diameter 3.2 mm and thickness of 1.8–2.5 mm) were obtained by thermal pressing the ferrite/alloy/polymer mixture into a brass die under a pressure of 5 MPa and a temperature of 145 °C. Complex permeability was measured on final samples by a combined impedance/network analysis method. The dc electrical conductivity was determined using standard two-probe procedure.

3. Results and discussion

The plots of complex permeability $\mu = \mu' - j\mu''$ versus frequency f for bulk FeSiAl alloy and LiZnTi ferrite are shown in Fig. 1. The real part (μ') of μ in FeSiAl alloy is about 203 at a frequency of 100 Hz and then after a small rise it drops sharply to a very small value. The imaginary part (μ'') reaches a peak value of 224 at $f_1 = 316$ Hz. On the other hand, the μ' in LiZnTi ferrite has a constant value of 92 at first then attains a certain growth followed by a steep decline. The μ'' showed two peak values, the first about 55 at $f_1 = 16$ MHz and the second around 9 at $f_2 = 655$ MHz. A small negative value of μ' was observed between 2.3 and 6 GHz as depicted in the inset of Fig. 1.



Fig. 1. Complex permeability vs. frequency for bulk FeSiAl alloy and LiZnTi ferrite. The inset shows the detail for LiZnTi ferrite in GHz frequency region.

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In magnetic materials, the frequency variation of permeability is related with its dispersion and can be explained by magnetic resonance and eddy current effect. The former is due to the domain wall oscillation at low frequency (f_1) and the spin precession or natural ferromagnetic resonance at higher frequency (f_2) . The latter is caused by formation of magnetic moments due to eddy currents flowing on the surface of metallic material. Because FeSiAl alloy is conductive (with dc conductivity $\sigma_{dc} = 7.9 \times 10^5 \text{ Sm}^{-1}$), the eddy current effect is responsible for the abrupt decrease of permeability with frequency. The eddy currents bring about the drop of an effective volume contributing to the permeability of material thanks to the fall of the skin depth $\delta \approx \sqrt{1/(\pi f \sigma_{dc} \mu_o \mu')}$ [3]. Since the abrupt decrease of μ' can happen above the frequency, at which δ starts to be smaller than the sample thickness $(d \approx 2 \text{ mm})$, it is possible to estimate this frequency, f_{eddy} , as $f_{eddy} \approx$ $1/(\pi\sigma_{dc}\mu_o\mu'd^2)$. Calculated value of $f_{eddy} \approx 396$ Hz for FeSiAl alloy is close to the peak frequency $f_1 = 316$ Hz of $\mu''-f$ dependence. In case of LiZnTi ferrite, the low frequency maximum of μ'' (at f_1) corresponds to the domain wall resonance while the high frequency one (at f_2) indicates the natural ferromagnetic resonance. The negative value of μ' in the inset of Fig. 1 originates from the magnetic resonance owing to the internal magnetic anisotropy field. Note that due to the low conductivity of LiZnTi ferrite ($\sigma_{dc} = 5 \times 10^{-12} \text{ Sm}^{-1}$), the contribution of eddy current effect can be neglected.



Fig. 2. Real part and imaginary part (inset) of complex permeability vs. frequency for synthesized composites.

The μ -f plots of LiZnTi/FeSiAl/PVC composites can be found in Fig. 2. The μ' at low frequency (1 MHz) in composite samples decreases from 12.2 for LiZnTi/PVC composite to 6.9 for FeSiAl/PVC one. The type of frequency dispersion of μ changes from resonance one, reached in LiZnTi/PVC sample, to relaxation one observed in FeSiAl/PVC composite. The ferrite/polymer composite exhibited three resonance maxima in $\mu''-f$ dependence as can be seen in the inset of Fig. 2: the first at $f_1 = 36$ MHz (which corresponds to f_1 in LiZnTi ferrite), the second at $f_2 = 268$ MHz and the third at $f_3 = 697$ MHz (which is near f_2 in LiZnTi ferrite). On the other hand, the metal alloy/polymer composite achieved only one peak in $\mu''-f$ plot at $f_1 = 319$ MHz and it is assumed that this peak is due to the coincidence of both magnetic resonances (domain wall and natural ferromagnetic one). In this composite, the influence of eddy currents cannot be neglected since the largest particle size 160 μ m is much higher than the skin depth $\delta \approx 2.3 \ \mu m$ at 300 MHz and approximated value of $f_{eddy} \approx 458$ MHz is slightly behind the $f_1 = 319$ MHz. It should be noted that composites with the mixture ratios of hybrid LiZnTi: FeSiAl filler 0.75:0.25, 0.50:0.50 and 0.25:0.75 reached two maximum values in $\mu''-f$ plots: the first is between f_2 of LiZnTi/PVC sample and f_1 of FeSiAl/PVC one, and the second is around f_3 of LiZnTi/PVC composite. Unlike bulk samples, the differences exhibited in μ -f dependences for composites are direct consequence of demagnetizing effects in filler particles: μ' decreased and resonance frequencies f_1 , f_2 shifted towards higher values due to the contribution of demagnetizing field. Moreover, the change of the filler mixture ratio in composites led to the alternation of magnetocrystalline anisotropy and accordingly also the values of μ' and f_1, f_2 .

4. Conclusions

The LiZnTi/FeSiAl/PVC composites with variable hybrid filler mixture ratio were prepared by thermal pressing method and the frequency variation of complex permeability was measured and analyzed. Whereas bulk samples (LiZnTi ferrite and FeSiAl alloy) showed the resonance type of permeability dispersion, the composites exhibited both the resonance and relaxation one. The dispersion of permeability was due to the domain wall and natural ferromagnetic resonance phenomena. The eddy currents affected the permeability too, especially in samples with higher content of conductive magnetic filler.

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