

Effects of the Non-Homogeneity and Elastic Medium on the Critical Torsional Load of the Orthotropic Cylindrical Shell*

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In this study, the torsional stability problem of non-homogeneous orthotropic composite cylindrical shells in the elastic medium, using the Galerkin method was investigated. The Winkler model is used to describe the reaction of the elastic medium on the cylindrical shell. Mixed boundary conditions are considered. The effects of variations of shell parameters, non-homogeneity, orthotropy and foundation stiffness on the critical torsional load are examined.

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1. Introduction

In recent years, non-homogeneous composite shell structures are widely used in modern engineering structures such as tunnels, storage tanks, pressure vessels, water ducts, pipelines, and casing pipes, process equipment and in other applications. Such shells are usually laid on or placed in a soil medium as an elastic foundation, thus there is a great interest in stability analysis of cylindrical shells on the elastic foundation. The non-homogeneity of materials stems from production techniques, surface and thermal polishing processes, effect of radiation, etc. Thus, the mechanical properties of materials change from point to point as continuous functions of coordinates [1, 2]. Currently, some investigations on the stability analysis of cylindrical shells resting on the elastic foundation have been published in the open literature [3]. There are some important publications related to the torsional stability of composite shells [4]. Hence, the stability of non-homogeneous orthotropic cylindrical shells surrounded by an elastic medium and subjected to torsional load has not been studied enough, analytically. In the current study, an attempt is made to address this problem. The basic equations of non-homogeneous orthotropic cylindrical shells resting on the Winkler elastic foundation are derived and closed form solution is obtained. The results reveal that variations of the cylindrical shell parameters, the non-homogeneity, the orthotropy of material and the Winkler foundation stiffness have significant effects on the values of the critical torsional load.

2. Problem description and basic equations

As shown in Fig. 1, a thin non-homogeneous orthotropic circular cylindrical shell surrounded by an elastic medium and subjected to the uniform torsional load, S , is considered. The cylindrical shell is of length L , thickness h , and radius R . The origin of the coordinate system is taken as the left side of length of the reference surface of the cylindrical shell. The x axis is taken along a generator, y axis is taken tangential directions and ζ axis normal to them. The axes of orthotropy are parallel to x and y axes. The Winkler model is used to describe the reaction of the elastic medium on the cylindrical shell and K_w (in N/m^3) is the Winkler foundation stiffness.

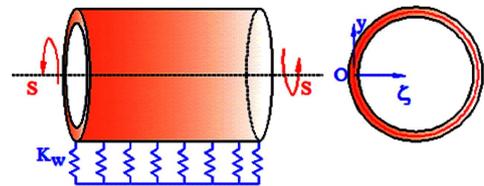


Fig. 1. Geometry of an orthotropic cylindrical shell on the Winkler elastic foundation and under torsion.

The non-homogeneity of orthotropic material of the shell is assumed to arise due to the exponential variation of Young's moduli along the thickness direction ζ as [1, 2]:

$$\begin{aligned} E_1(\bar{\zeta}) &= E_{01} e^{\mu(\bar{\zeta}-0.5)}, & E_2(\bar{\zeta}) &= E_{02} e^{\mu(\bar{\zeta}-0.5)}, \\ G(\bar{\zeta}) &= G_0 e^{\mu(\bar{\zeta}-0.5)}, & \bar{\zeta} &= \zeta/h, \end{aligned} \quad (1)$$

where E_{01} and E_{02} are the Young moduli in x and y directions, respectively, G_0 is the shear modulus, μ is the exponential factor characterizing the degree of material gradient in ζ direction and satisfies $-1 \leq \mu \leq 1$. We remark that $\mu = 0$ corresponds to the homogeneous case, $\mu < 0$ to the graded soft material, and $\mu > 0$ to the graded stiff material.

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TABLE

The variation of critical torsional loads and (n_{cr}, γ_{cr}) , for H and NH orthotropic cylindrical shells on the Winkler elastic foundation versus R/h , L/R , E_{01}/E_{02} and μ for $K_w = 5 \times 10^6 \text{ N/m}^3$.

R/h	$S_{cr}^{NH}/10^8 \text{ Pa}(n_{cr}, \gamma_{cr}), \mu = 0.5$				$S_{cr}^{wNH}/10^8 \text{ Pa}(n_{cr}, \gamma_{cr}), \mu = 0.5$			
	$L/R = 0.5$	$L/R = 1$	$L/R = 2$	$L/R = 3$	$L/R = 0.5$	$L/R = 1$	$L/R = 2$	$L/R = 3$
75	2.222(0.32, 12)	0.784(0.33, 8)	0.423(0.31, 7)	0.346(0.27, 6)	2.252(0.32, 12)	0.839(0.34, 9)	0.508(0.36, 8)	0.441(0.35, 7)
100	1.299(0.32, 13)	0.499(0.33, 9)	0.293(0.30, 8)	0.244(0.26, 7)	1.345(0.33, 13)	0.577(0.36, 10)	0.395(0.38, 9)	0.362(0.38, 9)
125	0.864(0.32, 13)	0.356(0.32, 10)	0.222(0.28, 8)	0.189(0.27, 8)	0.930(0.34, 14)	0.454(0.38, 11)	0.342(0.41, 10)	0.321(0.41, 10)
R/h	$S_{cr}^H/10^8 \text{ Pa}(n_{cr}, \gamma_{cr}), \mu = 0$				$S_{cr}^{wH}/10^8 \text{ Pa}(n_{cr}, \gamma_{cr}), \mu = 0$			
75	2.857(0.32, 12)	1.006(0.33, 8)	0.541(0.31, 7)	0.442(0.27, 6)	2.887(0.32, 12)	1.063(0.34, 9)	0.629(0.35, 7)	0.542(0.34, 7)
100	1.671(0.32, 13)	0.640(0.33, 9)	0.375(0.30, 8)	0.313(0.26, 7)	1.717(0.33, 13)	0.721(0.35, 10)	0.484(0.37, 9)	0.441(0.37, 9)
125	1.111(0.32, 13)	0.457(0.32, 10)	0.284(0.28, 8)	0.242(0.27, 8)	1.178(0.33, 14)	0.558(0.37, 11)	0.411(0.39, 10)	0.384(0.40, 10)
$S_{cr}/10^8 \text{ Pa}(n_{cr}, \gamma_{cr}), R/h = 100, L/R = 2$								
E_{01}/E_{02}	NH ($\mu = 0.5$)	H	wNH ($\mu = 0.5$)	wH	μ	NH	wNH	
5	1.031(0.22, 8)	1.321(0.22, 8)	1.183(0.25, 9)	1.483(0.25, 9)	-1.0	0.624(0.30, 8)	0.744(0.34, 8)	
25	0.426(0.18, 9)	0.545(0.18, 9)	0.549(0.23, 10)	0.672(0.22, 10)	0	0.375(0.30, 8)	0.484(0.37, 9)	
50	0.292(0.17, 10)	0.374(0.17, 10)	0.406(0.22, 11)	0.493(0.21, 11)	1.0	0.229(0.30, 8)	0.327(0.39, 9)	

Stress-strain relations for thin non-homogeneous orthotropic cylindrical shells are

$$\begin{pmatrix} \sigma_{11} \\ \sigma_{12} \\ \sigma_{12} \end{pmatrix} = \begin{bmatrix} Q_{11} & Q_{12} & 0 \\ Q_{21} & Q_{22} & 0 \\ 0 & 0 & Q_{66} \end{bmatrix} \begin{bmatrix} e_{11} - \zeta w_{,xx} \\ e_{12} - \zeta w_{,yy} \\ e_{12} - 2\zeta w_{,xy} \end{bmatrix}, \quad (2)$$

where σ_{ij} ($i, j = 1, 2$) are the stress components, e_{ij} ($i, j = 1, 2$) are the strain components on the reference surface, w is the displacement of the reference surface in the normal direction and assumed to be much smaller than the thickness, and coma indicates the partial derivative. The quantities Q_{ij} , $i, j = 1, 2, 6$ are given in Refs. [1, 2].

The basic equations of non-homogeneous orthotropic cylindrical shells under torsional load and resting on the Winkler elastic foundation can be obtained as

$$\begin{aligned} c_{12} \Psi_{,xxxx} + (c_{11} - 2c_{31} + c_{22}) \Psi_{,xxyy} + c_{21} \Psi_{,yyyy} \\ + \frac{1}{R} \Psi_{,xx} - c_{13} w_{,xxx} - (c_{14} + 2c_{32} + c_{23}) w_{,xxy} \\ - c_{24} w_{,yyy} - 2Shw_{,xy} + K_w w = 0, \end{aligned} \quad (3)$$

$$\begin{aligned} b_{22} \Psi_{,xxxx} + (b_{12} + 2b_{31} + b_{21}) \Psi_{,xxyy} + b_{11} \Psi_{,yyyy} \\ - b_{23} w_{,xxx} - (b_{13} - 2b_{32} + b_{24}) w_{,xxy} \\ - b_{14} w_{,yyy} + \frac{1}{R} w_{,xx} = 0, \end{aligned} \quad (4)$$

where c_{ij}, b_j ($j = 1, 2, \dots, 4$) are non-homogeneous orthotropic shell characteristics [2].

3. Solution of the problem

The edge conditions of the cylindrical shell are mixed boundary conditions. The solution of Eqs. (3) and (4) is sought in the following form [5]:

$$\begin{aligned} w &= \xi_1 \sin \frac{\pi x}{L} \sin \frac{n}{R} (y + \gamma x), \\ \Psi &= \xi_2 \sin \frac{\pi x}{L} \sin \frac{n}{R} (y + \gamma x), \end{aligned} \quad (5)$$

where $m_1 = \pi R/L$, n is the wave number in the direction of y axis, γ is tangent of the angle between the waves and x axis, ξ_1 and ξ_2 are amplitudes [4, 5].

Substituting Eq. (5) into Eqs. (3) and (4), and then applying the Galerkin method, the expression for the critical torsional load (in MPa) of non-homogeneous orthotropic cylindrical shells resting on the Winkler elastic foundation is obtained

$$\begin{aligned} S_{cr}^{wNH} &= \frac{1}{2hn^2\gamma R^2} \left\{ \left[R(\gamma^2 n^2 + m_1^2) \right. \right. \\ &\quad - c_{12} (m_1^4 + (c_{21}/c_{12})n^4 + 6m_1^2 n^2 \gamma^2 + n^4 \gamma^4) \\ &\quad \left. \left. - (c_{11} - 2c_{31} + c_{22}) (n^4 \gamma^2 + m_1^2 n^2) \right] \right. \\ &\quad \times \left[b_{23} (m_1^4 + (b_{14}/b_{23})n^4 + 6m_1^2 n^2 \gamma^2 + \gamma^4 n^4) \right. \\ &\quad \left. + (b_{13} - 2b_{32} + b_{24}) (n^4 \gamma^2 + m_1^2 n^2) \right. \\ &\quad \left. + (\gamma^2 n^2 + m_1^2) R \right] \\ &\quad \left/ \left[b_{22} (m_1^4 + (b_{11}/b_{22})n^4 + 6m_1^2 n^2 \gamma^2 + \gamma^4 n^4) \right. \right. \\ &\quad \left. \left. + (b_{12} + 2b_{31} + b_{21}) (n^4 \gamma^2 + m_1^2 n^2) \right] \right. \\ &\quad \left. + c_{13} (6m_1^2 n^2 \gamma^2 + m_1^4 + (c_{24}/c_{13})n^4 + \gamma^4 n^4) \right. \\ &\quad \left. + (c_{14} + 2c_{32} + c_{23}) (n^4 \gamma^2 + m_1^2 n^2) + K_w R^4 \right\}. \end{aligned} \quad (6)$$

The minimum values of the critical torsional load are obtained by minimizing Eq. (6) with respect to (n, γ) .

4. Numerical examples and discussions

Numerical examples, for the homogeneous (H) and non-homogeneous (NH) orthotropic cylindrical shells with or without Winkler elastic foundation are presented in Table. The calculations were performed for the ratio E_{01}/E_{02} , and $E_{01} = 2 \times 10^{11} \text{ Pa}$, $\nu_{12} = 0.3$ are taken into account [2]. In all the other computations, boron-epoxy composite with the following orthotropic material properties are considered: $E_{01} = 2.06844 \times 10^{11} \text{ Pa}$, $E_{02} = 1.86159 \times 10^{10} \text{ Pa}$, $G_0 = 4.48162 \times 10^9 \text{ Pa}$, $\nu_{12} = 0.21$, $\nu_{21} = 0.0189$ [6]. As the ratios R/h , L/R , E_{01}/E_{02} and exponential factor μ increase, the values of the critical

torsional load and the effect of non-homogeneity decrease for the H and NH orthotropic cylindrical shells with or without an elastic foundation. The effect of the elastic foundation on the critical torsional loads increases, as R/h , L/R , E_{01}/E_{02} and μ increase. It is seen that $S_{cr}^{NH} > S_{cr}^H$ for the soft material, whereas, $S_{cr}^{NH} < S_{cr}^H$ for the stiff material.

5. Conclusions

In this study, the torsional stability problem of non-homogeneous orthotropic composite cylindrical shells on the elastic foundation, using the Galerkin method was investigated. The Winkler model is used to describe the reaction of the elastic medium on the cylindrical shell. Mixed boundary conditions are considered. The effects of variations of shell parameters, non-homogeneity, orthotropy and foundation stiffness on the critical torsional load are examined.

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