

Proceedings of the International Congress on Advances in Applied Physics and Materials Science, Antalya 2011

Investigation of Behaviour of Titanium Diboride Reinforced Boron Carbide–Silicon Carbide Composites against Cs-137 Gamma Radioisotope Source by Using Gamma Transmission Technique

B. BUYUK^a, A.B. TUGRUL^a, A.C. AKARSU^b AND A.O. ADDEMIR^b

^aITU Energy Institute — Nuclear Research Division, Ayazaga Campus 34669, Maslak/Istanbul, Turkey

^bITU Metalurgical and Materials Engineering Faculty, Ayazaga Campus 34669, Maslak/Istanbul, Turkey

Boron carbide is a material which has wide application areas in industry including nuclear technology. Titanium diboride reinforced boron carbide–silicon carbide composites were studied for searching of the behaviour against the gamma ray. It has been adopted that depending on their properties such improved materials can be used in nuclear technology. For the investigation of the gamma radiation behaviour of these materials, Cs-137 radioisotope was used as gamma source in the experiments which have a single gamma-peak at 0.662 MeV. Gamma transmission technique was used for the measurements. Different reinforcing ratios, titanium diboride reinforced boron carbide–silicon carbide composites were evaluated in relation to gamma transmission and the results of the experiments were interpreted and compared with each other. It could be understood that the increasing ratio of titanium diboride in boron carbide–silicon carbide composites causes higher hardness, strength and linear attenuation coefficient values but decrease the mass attenuation coefficient.

PACS: 25.20.Dc

1. Introduction

Boron carbide is a material that is used in wide application areas in industry. Some of these areas are the nuclear technology, military industry, ceramic industry and air-space industry [1, 2]. Boron carbide has low-density, high hardness and corrosion resistance, chemical stability and high neutron capture feature [2]. Some boron carbide application fields are lightweight ceramic armor, sand blasting nozzles, nuclear reactors, reactor control rods and the radiation shielding materials [2, 3]. However, boron carbide is brittle, has low strength and high temperature sintering properties [3, 4]. Since the sintering of pure boron carbide to high densities is difficult, specific additives such as SiC, Al₂O₃, TiB₂, AlF₃, W₂B₅, elemental boron and carbon have been used as sintering aids to increase the sintered density [2–5].

In this study, titanium diboride reinforced with boron carbide–silicon carbide composites were studied for searching of the behaviour against the gamma ray. For the investigation of the gamma radiation behaviour of these materials, Cs-137 radioisotope was used as gamma source in the experiments which has a single gamma-peak at 0.662 MeV and half life is 30.1 y [6, 7].

Gamma transmission technique was used for the measurements. Experimental geometry and experimental setup were prepared carefully and scattering effect was minimized. In the experiments, PM1401K model, scintillation detector and multi-channel analyzer, was used for the measurement of the gamma peak. All the measurements were implemented by taking at least three counts in the same geometry.

Different reinforcing ratios, titanium diboride reinforced with boron carbide–silicon carbide composites, were evaluated in relation to gamma transmission and the

results of the experiments were interpreted and compared with each other. Therefore, the behavior of titanium diboride reinforced boron carbide–silicon carbide composites were investigated against Cs-137 gamma radioisotope source by using gamma transmission technique.

2. Experiments and materials

Gamma transmission technique is based on penetrating gamma rays through materials. Detector and gamma source were put on both sides of the material within the same axis. Then gamma radiation counts are measured reaching the detector from the source are measured. The counts with material and without material are compared and evaluate [6–8]. Figure 1 shows schematic view of gamma transmission technique.

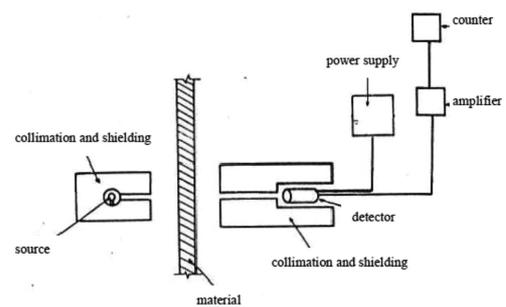


Fig. 1. Schematic view of gamma transmission technique.

The radiation passing through the material is calculated by the following equation:

$$I = I_0 e^{-\mu x}, \quad (1)$$

where I and I_0 are the transmitted and initial gamma ray

intensities, respectively, μ is linear attenuation coefficient of material at specific γ -ray and x is the thickness of the material.

The materials which were used in the experiments have different titanium diboride ratios in the composites. Thus they are coded according to their titanium diboride ratios by volume in composites. Table I shows the materials used in the experiments and their ratios by volume in the composite materials and also their hardness, strength and density properties [5].

All composite materials were sintered at 2250 °C for 2 h under 130 MPa pressure. The materials which were used in the experiments have about $1 \times 0.5 \times 2$ cm³ dimensions. Cs-137 gamma radiation source which has 8.9 μ Ci was used in the experiments. Lead blocks were used for radiation shielding and collimation. The collimator diameter is 7 mm. The distance between the detector and source is 10 cm. Firstly, the background radiation was measured. Then Cs-137 gamma source was set. Initial intensity count (I_0) was measured. Then materials were set and intensity counts (I) were measured for all thickness values. All counts were measured three times for 600 s and net counts calculated by reducing background value. Average values and standard deviations were calculated. For rational evaluating, relative intensity (I/I_0) values were calculated. Results were given with tables. Relative intensity–material thickness graph was drawn for each titanium diboride ratio. Exponential distribution was shown on graphs and exponential equations were calculated. Then results were evaluated and discussed.

3. Experimental results

Results for titanium diboride free boron carbide–silicon carbide composites, 2% (by volume) titanium diboride reinforced boron carbide–silicon carbide composites and 4% (by volume) titanium diboride reinforced boron carbide–silicon carbide composites are given in Table II.

Using the values in the tables relative intensity–material thickness graphs were drawn for all titanium diboride ratios. Exponential fitted equations were calculated. Figure 2 shows all titanium diboride reinforced boron carbide–silicon carbide composites comparatively.

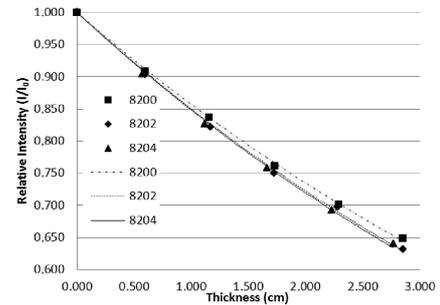


Fig. 2. Relative intensity for titanium diboride reinforced boron carbide–silicon carbide composites.

4. Discussion and conclusion

The linear attenuation coefficients (μ) of all materials were calculated by using Fig. 2. The correlation coefficients of results are $R^2 = 0.999$ and 0.998 and 0.998 , respectively. The mass attenuation coefficients ($\mu_m = \mu/\rho$) of the materials were also calculated. Finally, the mass attenuation coefficients of the composites were compared with the theoretical values which were calculated from XCOM computer code [9].

Table III shows the linear and mass attenuation coefficients for the composite materials and % difference of experimental and theoretical mass attenuation coefficient values of the studied materials. It could be said that theoretical and experimental mass attenuation coefficients are of same tendency and close to each other. The difference percentage is about 6–8%.

TABLE I

The contents and the properties of the composite materials which were used in the experiments [5].

Material (code)	B ₄ C [% volume]	SiC [% volume]	TiB ₂ [% volume]	Hardness [Vickers]	Strength [MPa]	Density [g/cm ³]
8200	80	20	0	1777.6 ± 93.22	218.925 ± 29.14	2.244
8202	78.4	19.6	2	1902.57 ± 131.8	261.425 ± 25.60	2.361
8204	76.8	19.2	4	1983.67 ± 56.78	276.125 ± 78.79	2.429

TABLE III

The linear and mass attenuation coefficients of 8200, 8202 and 8204 composite materials.

Material (code)	Linear attenuation coefficient [cm ⁻¹]	Mass attenuation coefficient [10 ⁻² cm ² /g]		
		Experimental	XCOM	% Difference
8200	0.154	6.863	7.359	6.744
8202	0.162	6.862	7.355	6.710
8204	0.165	6.793	7.352	7.605

TABLE II

Results for titanium diboride reinforced and without reinforced boron carbide–silicon carbide composites with Cs-137 gamma source.

Materials	Accumulation time = 600 s						
	Thickness [cm]	Net count 1	Net count 2	Net count 3	Average count	Standard deviation	Relative count
8200	0	8047	8132	8056	8079	47	1.000
	0.598	7325	7361	7330	7339	19	0.908
	1.156	6723	6754	6791	6756	34	0.836
	1.729	6111	6153	6185	6150	37	0.761
	2.291	5649	5689	5663	5667	20	0.701
	2.855	5267	5215	5235	5239	26	0.648
8202	0.000	8135	8128	8211	8158	46	1.000
	0.594	7372	7393	7320	7362	38	0.902
	1.169	6654	6652	6780	6695	73	0.821
	1.724	6147	6121	6073	6114	37	0.749
	2.283	5736	5689	5621	5682	58	0.696
	2.853	5116	5196	5119	5144	45	0.631
8204	0	8135	8128	8116	8127	10	1.000
	0.571	7346	7297	7367	7337	36	0.903
	1.119	6718	6696	6725	6713	15	0.826
	1.664	6163	6121	6171	6152	27	0.757
	2.229	5610	5656	5590	5619	34	0.691
	2.769	5209	5198	5192	5200	8	0.640

It could be understood that the increasing ratio of titanium diboride in boron carbide–silicon carbide composites causes higher hardness, strength and linear attenuation coefficient values but decreases the mass attenuation coefficient. The mass attenuation coefficients are close to theoretical values. On the other hand, the production techniques of composite materials are very important. As a result, it was concluded that increase of the ratio of titanium diboride in the boron carbide–silicon carbide composites causes increase of gamma attenuation of the composites. Therefore, titanium diboride reinforced boron carbide–silicon carbide composites can be used in nuclear technology as a shielding material because of their improved hardness, strength and linear attenuation coefficient values.

Acknowledgments

The authors wish to thank BMBT Co. to their support about production of materials.

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