Properties of Acoustic Emission Signals Coming from Partial Discharges Caused by Modeled Sources Immersed in Transformer Oil

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Investigation results concerning acoustic emission signals coming from partial discharges generated by modeled sources are presented in the paper. These sources have been made using different bushing ends (without any extra elements and with a thread or a pike) situated directly in the oil, but without screens typical for partial discharge investigations in a bushing. Measurements have been carried out using own measuring acoustic emission system DEMA-COMP and — in a parallel way — computer-aided partial discharges measuring system TE 571 (produced by the firm Haefely Trench). Fundamental and advanced analysis of acoustic emission signals has been made. These signals were recorded in 20 measuring situations which need to multiple installation of acoustic emission sensors. Conclusions resultant from own originate advanced analysis of signals content description of properties revealed by defined acoustic emission descriptors.

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1. Description of modeled sources, a measuring stand and measuring systems

As a modeled partial discharges (PD) source, made and used during the investigations, was the bushing PTK 123/450/630 with additional ends (without any extra elements, with a thread or a pike) situated directly in the oil. This bushing was not equipped with screens typical for PD investigations.

Investigations of PD generated by modeled sources have been carried out in High Voltage Laboratory of the firm ZTS IZO-ERG in Gliwice and precisely — on the measuring stand presented in Fig. 1. An integral element of this stand is the vat in shape of the cylinder (diameter of 900 mm, height of 1200 mm). PD sources have been placed inside the vat filled by the oil. Such PD sources and measuring conditions enable us to observe partial discharges in boundary of the voltage electrode and transformer oil as well as only in the oil.

Acoustic emission (AE) sensors have been placed during investigations at measuring points P_A , P_B and P_C on external surface of the vat within specially prepared clamps. Permanent magnets (elements of sensor clamps) ensured unchangeable position of sensors on vat walls during measurements as well as recurrent thickness of the couple layer (it is the cup grease which ensures good conditions of acoustic contact). Measurements have been carried out using in a parallel way own measuring AE system DEMA-COMP [1–8] and computer-aided PD mea-

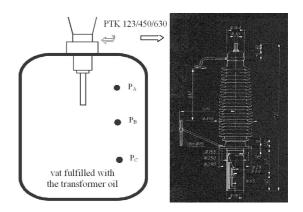


Fig. 1. Scheme of measuring stand used to investigate of PDs generated by modeled sources immersed in the oil fulfilling the vat; P_A , P_B , P_C — measuring points fixed on external surface of the vat.

suring system TE 571, produced by the firm Haefely Trench (investigations of other authors are published in [9–18]).

Distances between a modeled source and AE sensors are of several tens of centimeters. These distances are typical for AE signals, generated in many real objects. Owing to that, results of analyses carried out for AE signals recorded in such a way have also technical value.

Investigations have been made using the following methodology:

1. modeled PD source was introduced into the vat and then maximum of the supply voltage used during the measurements was determined experimentally,

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- 2. AE sensors were installed at measuring points $P_{\rm A},$ $P_{\rm B},$ $P_{\rm C},$
- 3. measurements of PD and apparent charge were carried out for selected supply voltages,
- 4. every investigation has been repeated for a successive modeled source.

Globally, signals have been recorded in 20 measuring situations. Measuring conditions and input data necessary to analyze are presented in Table I. It should emphasize that recorded measuring data (also in the same measuring path) are obtained in results of montage of AE sensor which is repeated three times. That causes fluctuations of couple layer dimensions. Therefore, presented analysis of AE signals concerns a complex situation where data are result of repeated installation of AE sensors.

TABLE I List of measuring conditions and data for analysis.

No. Source U [kV] Q [pC] File 1 bushing 123 1260 TP11(1) 2 bushing 140 1000 TP17(1) 3 bushing 130 890 TP14(1)										
No.	Source	U [kV]	Q [pC]	File						
1	bushing	123	1260	TP11(1)						
2	bushing	140	1000	TP17(1)						
3	bushing	130	890	TP14(1)						
4	bushing	106	220	TP8(1)						
5	bushing	90	90	TP5(1)						
6	bushing	74	50	TP3(1)						
7	bushing	60	10	TP1(1)						
8	bushing	0	10	TSZ1(1)						
9	b+point	106	280	TO16(1)						
10	b+point	90	180	TO12(1)						
11	b+point	74	100	TO7(1)						
12	b+point	50	10	TO1(1)						
13	b+point	0	10	TOS1(1)						
14	b+thread	123	500	TG89(1)						
15	b+thread	106	450	TG85(1)						
16	b+thread	90	360	TG81(1)						
17	b+thread	74	220	TG77(1)						
18	b+thread	60	25	TG73(1)						
19	b+thread	50	10	TG70(1)						
20	b+thread	0	10	TGS3(1)						

2. Fundamental characteristics of AE signals coming from PD generated by modeled sources immersed in transformer oil

Fundamental characteristics calculated for example AE signals, presented in Figs. 2–5, are as follows:

- phase-time characteristic with minimum, maximum and root mean square (RMS) of the signal, as in Figs. 2–5a (for filtration a band-pass filter of five order was used, filtration band is done as frequency interval at frequency characteristic),
- three-dimensional spectrogram STFT, as in Figs. 2–5b,

- averaging phase characteristic, as in Figs. 2–5c,
- spectral power density as frequency characteristic of a signal with the frequency for main maximum and value of the spectrum for this frequency, as in Figs. 2–5d.

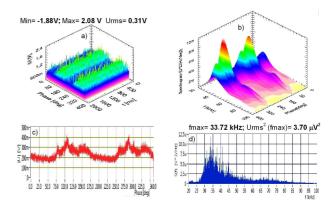


Fig. 2. Fundamental description of the AE signal: (a) phase-time characteristic, (b) averaging STFT spectrogram, (c) averaging phase characteristic, (d) frequency characteristic recorded in measuring conditions: bushing with end without any extra elements, 1000 pC, 140 kV, measuring line K2 (40 dB, R6#2), measuring position $P_{\rm B}$ — TP17(1) file.

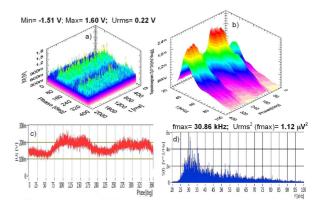


Fig. 3. Fundamental description of the AE signal: (a) phase–time characteristic, (b) averaging STFT spectrogram, (c) averaging phase characteristic, (d) frequency characteristic, recorded in measuring conditions: bushing with end including the thread, 500 pC, 123 kV, measuring line K2 (40 dB, R6#2), measuring position $P_{\rm B}$ — TG69(1) file.

In the consequence of analysis, the whole range of measured apparent charge $Q_{\rm p}$ (generated by modeled PD sources) has been divided to three intervals: up to 220 pC, from 220 pC to 500 pC and below 500 pC; such intervals were assigned the symbols A, B and C. Conclusions resultant from analysis of signals are as follows:

 AE signals have simultaneously periodic and random character (Figs. 2–5a),

Min= -0.20 V; Max= 0.20 V; Urms= 0.04 V

Fig. 4. Fundamental description of the AE signal: (a) phase-time characteristic, (b) averaging STFT spectrogram, (c) averaging phase characteristic, (d) frequency characteristic, recorded in measuring conditions: bushing with end including the thread, 500 pC, 123 kV, measuring line K2 (40 dB, R6#2), measuring position $P_{\rm B}$ — TO7(1) file.

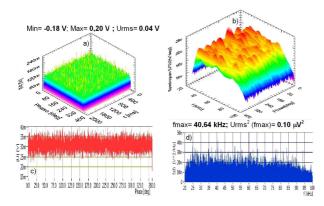


Fig. 5. Fundamental description of the AE signal: (a) phase-time characteristic, (b) averaging STFT spectrogram, (c) averaging phase characteristic, (d) frequency characteristic, recorded in measuring conditions: bushing with end including the thread, 10 pC, 50 kV, measuring line K2 (40 dB, R6#2), measuring position $P_{\rm B}$ — TG70(1) file.

- there are double phase intervals in two halves of supply voltage period at averaging phase-time characteristic (Figs. 2–5c) which correspond to "corridors of high values" in Figs. 2–5a,
- there is a good located main band within AE signals (Figs. 2–5d),
- averaging spectrograms (Figs. 2–5b) show more detailed phase ranges of the main band and additional bands,
- absolute values of quantities at particular characteristics grow when apparent charge introduced by a modeled PD source increases.

TABLE II

Comparison of properties — in time domain — for recorded AE signals generated by noises and PD.

No.	Description of	Quantity	Unity	Calculation results			
	quantity			Tsz	TP11		
				10 pC	$1260 \ \mathrm{pC}$		
1	mean value of the voltage of the sig- nal	$U_{\rm av}$	mV	18.5	12.6		
2	mean standard deviation of the mean value of the voltage of the signal	S_U	mV	39.3	187.7		
3	mean value of the signal modulus	$ U _{\mathrm{av}}$	mV	15.5	150.6		
4	coefficient of the distribution	$S_U/ U _{\rm av}$		2.5	1.2		
5	maximal value of the voltage of the signal	$U_{\rm Max}$	mV	230.2	1664.4		
6	minimal value of the voltage of the signal	$U_{ m Min}$	mV	-203.8	-2021.2		
7	RMS value of the voltage of the signal	$U_{\rm rms}$	mV	38.4	192.5		

Results of quantitative comparison of properties revealed by measuring noises and a signal coming from PD are presented in Table II. Results of quantitative analysis in domain of signal time are presented in the column "Tsz 10 pC" of Table II. Mean value of signal amplitude is practically equal to zero. Mean value of signal modulus is 15.5 mV, whereas mean standard deviation of the mean value is 39.3 mV, so it is 2.5 times greater than the mean value. Such a situation shows very "flat" character of Gauss' curve, describing distributions of signal amplitudes — typical for noises of a measuring path. In order to compare results of analysis for signal coming from a modeled PD source, introduced apparent charge of 1260 pC, are placed in column "TP11 1260 pC" of Table II. Mean value of signal modulus is in this case of 150.6 mV (i.e. 10 times higher than for noises), and mean standard deviation of the mean value of the voltage is 187.7 mV. These results give already "high" Gauss' distribution for recorded signal amplitudes — typical for information, not for a noise.

3. Advanced characteristics of AE signals coming from PD generated by modeled sources immersed within transformer oil

Advanced analysis of AE signals in domain of threshold and frequency has been carried out. Advanced analysis of AE signals in threshold domain includes calculations of amplitude distributions and descriptors with acronyms ADC, ADP and ADNC, proposed by authors [10–12]. These descriptors describe advancing stage of an AE signal. Obtained results are presented in Table III and in

Fig. 6 (symbol a in Table means descriptor values, symbol r means coefficient of correlation which shows quality of approximation for each descriptors).

TABLE	III
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Selected	quantities	describing	PD	signals	\sin	thres	hol	d (domain.	
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	File	Q	U	$U_{\rm pp}$	$U_{\rm rms}$	AD	Р	AD	С	ADNC		
		[pC]	[kV]	[V]	[V]	a	r	a	r	a	r	
1	TP11(1)	1260	123	3.84	0.19	-2.3	0.99	-3.3	0.99	-3.6	0.99	
2	TP17(1)	1000	140	3.96	0.31	-2.3	1.00	-2.7	1.00	-2.8	1.00	
3	TP14(1)	890	130	4.17	0.26	-2.7	1.00	-3.2	1.00	-3.4	1.00	
4	TG89(1)	500	123	3.11	0.22	-3.0	1.00	-3.7	1.00	-3.9	1.00	
5	TG85(1)	450	106	2.79	0.15	-2.7	0.99	-3.7	0.97	-4.2	0.99	
6	TG81(1)	360	90	2.18	0.10	-3.8	0.99	-5.1	0.96	-5.8	0.99	
7	TO16(1)	280	106	1.77	0.06	-4.6	0.89	-7.3	0.86	-8.2	0.93	
8	TG77(1)	220	74	1.75	0.06	-3.3	0.94	-6.0	0.93	-6.3	0.94	
9	TP8(1)	220	106	0.67	0.06	-16.1	0.99	-17.1	0.98	-17.9	0.99	
10	TO12(1)	180	90	0.98	0.04	-8.77	0.97	-11.8	0.94	-13.6	0.97	
11	TO7(1)	100	74	0.42	0.04	-27.1	0.99	-27.5	0.98	-30.6	0.99	
12	TP5(1)	90	90	0.51	0.05	-21.8	0.98	-24.4	0.98	-24.7	0.98	
13	TP3(1)	50	74	0.60	0.05	-15.7	1.00	-19.0	0.99	-20.2	1.00	
14	TG73(1)	25	60	0.49	0.04	-22.8	0.97	-26.4	0.98	-28.0	0.98	
15	TP1(1)	10	60	0.39	0.04	-33.5	0.98	-31.1	0.97	-35.2	0.98	
16	TSZ1(1)	10	0	0.52	0.04	-16.8	0.99	-20.3	0.99	-21.9	1.00	
17	TO1(1)	10	50	2.91	0.04	-26.8	1.00	-28.7	0.99	-31.2	1.00	
18	TOS1(1	10	0	0.35	0.04	-30.8	0.99	-30.0	0.98	-33.6	0.99	
19	TG70(1)	10	50	0.38	0.04	-35.5	0.97	-31.2	1.00	-36.7	0.98	
20	TGS3(1)	10	0	0.36	0.04	-30.2	0.99	-30.2	0.99	-33.4	0.99	

It should be emphasized that signals in Table III are arranged according to apparent charge values introduced by PD source (columns 4). In practice, this means comparison of AE signals recorded during multiple installation of AE sensors for the bushing with different ends.

Tendencies to change of descriptor values depending on apparent charge $Q_{\rm p}$, introduced by PD source, are as follows:

- AE descriptor values grow when apparent charge $Q_{\rm D}$ increases,
- considerable fluctuations of AE descriptor values within the range of small values of this charge show that — in background of the noises — even single acoustic event can introduce a considerable change

in amplitude distribution,

— ADC descriptor among others reveals the most regular distribution of values depending on apparent charge $Q_{\rm p}$ (introduced by PD source).

Advanced analysis of AE signals in frequency domain includes identification and location of main maxima on frequency characteristics of signals. Identification and location of maxima has been made by "window" method, with approximating of the curves by means of threeparametrical Gauss' curve

$$y = A \exp(-(f - f_0)^2 / (2\Delta^2))$$
(1)

with the following parameters: A — amplitude, f_0 — frequency corresponding to a main maximum, Δ — standard deviation for Gauss' curve.

TABLE IV

Selected quantities describing PD signals in frequency domain.

					K2			K3					
File	Q	U	f_0	Δ	A	$f_{ m d}$	$f_{\rm g}$	f_0	Δ	A	$f_{\rm d}$	$f_{\rm g}$	
	[pC]	[kV]	[kHz]	[kHz]	$[UU/{\rm Hz}]$	[kHz]	[kHz]	[kHz]	[kHz]	[UU/Hz]	[kHz]	[kHz]	
TP11(1)	1260	123	34.8	6.8	3.7×10^{-7}	28	42	33.2	7.3	3.8×10^{-7}	26	41	
TP17(1)	1000	140	35.1	6.9	8.8×10^{-7}	28	42	33.2	7.6	8.6×10^{-7}	26	41	
TP14(1)	890	130	35.1	7.0	6.5×10^{-7}	28	42	33.3	7.6	6.5×10^{-7}	26	41	
TG89(1)	500	123	33.0	9.0	2.7×10^{-7}	24	42	31.6	7.9	3.0×10^{-6}	24	39	
TG85(1)	450	106	33.0	8.4	1.5×10^{-7}	25	41	31.4	8.4	2.0×10^{-7}	23	40	
TG81(1)	360	90	33.0	8.5	6.5×10^{-8}	24	41	31.7	8.4	7.0×10^{-8}	23	40	
TO16(1)	280	106	33.0	6.7	3.2×10^{-8}	26	40	29.4	5.6	2.0×10^{-8}	24	35	
TP8(1)	220	106	33.7	7.4	2.9×10^{-8}	26	41	32.0	8.0	3.7×10^{-8}	24	40	
TG77(1)	220	74	32.9	10.0	1.8×10^{-8}	23	43	31.8	11.0	2.3×10^{-8}	21	43	
TO12(1)	180	90	32.3	8.1	8.8×10^{-9}	24	40	28.9	7.1	8.2×10^{-9}	22	36	
TO7(1)	100	74	none					none					
TP5(1)	90	90	33.2	8.0	1.5×10^{-8}	25	41	31.8	9.3	2.1×10^{-8}	22	41	
TP3(1)	50	74	none					none					
TG73(1)	25	60	none					none					
TP1(2)	10	60	none					none					
TO1(1)	10	50	none					none					
TG70(1)	10	50	none					none					
TSZ1	0	0	none					none					
TOS1(1)	0	0	none					none					
TGS3(1)	0	0	none					none					

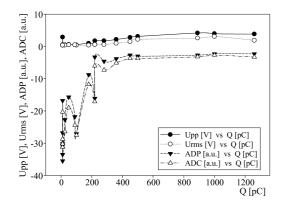


Fig. 6. Quantities describing AE signals registered in measuring channels K2 for different PD sources: bushing with the end without additional elements, bushing with sharp and bushing with thread.

Results of frequency analysis in Table IV show that frequency characteristics of PD signals obtained by means of AE method have the following properties:

- there is a lower limit of sensitivity on the level up to 100 pC,
- there is no visible dependence of main band posi-

tion on apparent charge value included by modeled source; signals belong to bands 23–43 kHz (measuring path K2) and 21–43 kHz (measuring path K3),

— signals recorded by AE sensor situated at larger distance from a modeled source have frequency band moved in direction of lower frequencies (in comparison with signals recorded by AE sensor situated at nearer distance from a modeled source) which results from comparison of parameters of signals recorded in two measuring paths.

4. Recapitulation

As a modeled PD source was the bushing with different additional ends (without any extra elements or with a thread and a pike) situated directly in the oil (without screens typical for investigations of PD in a bushing). Modeled PD sources enable us to observe partial discharges in boundary of the voltage electrode and also in the transformer oil.

Measurements have been carried out using — in a parallel way — own measuring AE system DEMA-COMP and computer-aided PD measuring system type TE 571, produced by the firm Haefely Trench. Globally, signals have been recorded in 20 measuring situations which need montage of AE sensors many times.

Fundamental and advanced analysis of recorded AE signals has been carried out.

Fundamental analysis leads to the following conclusions:

- AE signals have simultaneously periodic and random character,
- there are double phase intervals in two halves of supply voltage period which correspond to "corridors of high values" on phase-time characteristics,
- there is good located main band in AE signals,
- averaging spectrograms show more detailed phase ranges of the main band and additional bands,
- absolute values of quantities on particular characteristics grow when apparent charge introduced by a modeled PD source increases.

Advanced analysis of recorded signals give the following results:

- there is a visible dependence of main band position on the value of apparent charge introduced by a modeled source,
- comparison of parameters of signals recorded in two measuring paths shows that signals recorded by EA sensor situated at larger distance from a modeled source have frequency band moved in direction of lower frequencies,
- AE descriptors, allocated to AE signals the so--called advancing stage, arrange the signals and within a framework of analyzed group of AE signals it is arrangement similar to arrangement according to apparent charge Q; fluctuations are caused by additional phenomena which subjected AE waves during their propagation.

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